



## Dual Gate N-Channel Depletion Mode MOSFETS

### FEATURES

- Low Cost Plastic Package
- Monolithic Gate Protection Diodes
- Low Feedback Capacitance
- Silicon Nitride Passivation for Long Term Stability

### APPLICATIONS

TV Tuner RF Amplifiers and Mixers  
FM Tuner RF Amplifiers and Mixers  
IF Amplifiers  
Synchronous Detectors  
Wide Band RF Amplifiers

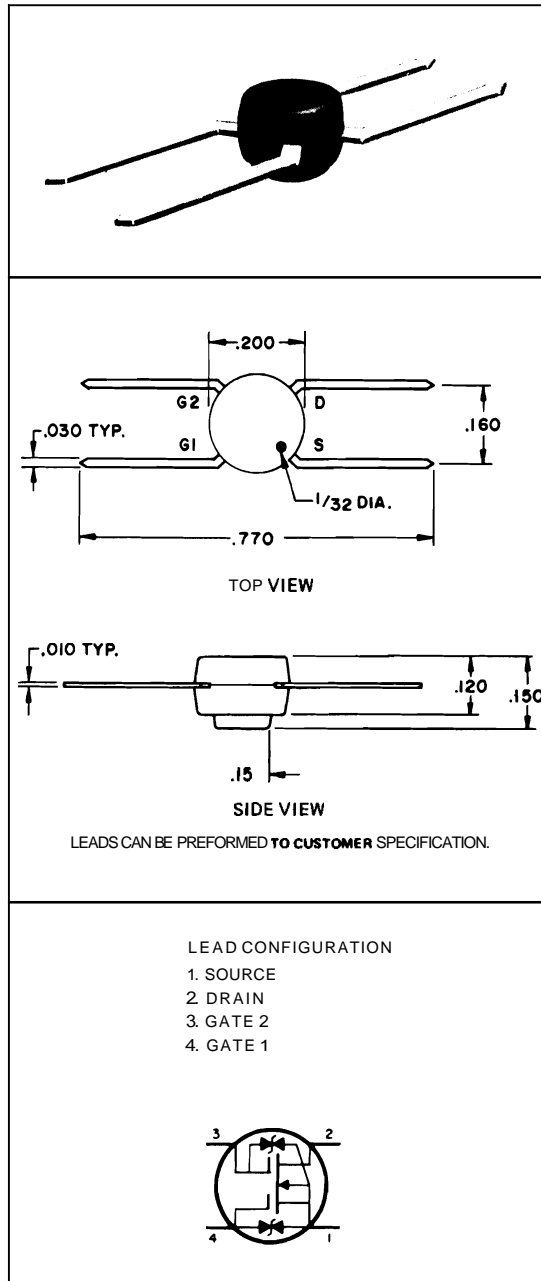
### DESCRIPTION

The MEM 6301 MEM 6311 MEM 632 are N-channel, Depletion Mode, Dual-Gate Metal Oxide Semiconductor transistors. They are protected from excessive input voltages by monolithic back-to-back diodes between gates and source.

The MEM 630 is intended for use in high frequency RF amplifiers of FM radios. Typical Gps of 22 dB and noise figure of 2.5 dB at 105 MHz.

The MEM 631 is intended for use in VHF amplifiers and high frequency tuned amplifiers such as TV tuners and 44 MHz or 10.7 MHz IF amplifiers. Typical Gps of 19 dB and noise figure of 3.5 dB at 200 MHz. Typical Gps of 30 dB and noise figure of 2.5 dB at 44 MHz.

The MEM 632 is intended for use in HF and VHF mixers. The high conversion gain makes the MEM 632 ideal for TV or FM tuner mixer applications. 105 MHz to 10.7 MHz Conversion Gain of 20 dB. 200 MHz to 44 MHz Conversion Gain of 17 dB.





## MAXIMUM RATINGS

Drain - Source Voltage	$V_{DS}$	25Vdc
Drain Current	$I_D$	30mAdc
Total Device Dissipation (Package Limitations)	$P_D$ @ $T_A = 25^\circ\text{C}$	500mW
Derate Above 25°C		5.0mW/°C
Operating and Storage Junction Temperature Range		-65 to +175 °C

ELECTRICAL CHARACTERISTICS ( $T_A=25^\circ\text{C}$  UNLESS OTHERWISE SPECIFIED)

SYMBOLS	CHARACTERISTICS	TEST CONDITIONS	MEM630			MEM631			MEM632			UNITS
			Min	Typ	Max	Min	Typ	M u	Min	Typ	M u	
BVDSX	Drain-Source Breakdown Voltage	$I_D=10\mu\text{A}$ , $V_S=0$ , $V_{G1}=V_{G2}=-4.0\text{V}$	20			20			20			volts
BVG1S0	Gate 1-Source Breakdown Voltage	$I_{G1}=\pm 10\mu\text{A}$ , $V_{G2S}=0$	$\pm 6.0$			$\pm 6.0$			$\pm 6.0$			volts
BVG2S0	Gate 2-Source Breakdown Voltage	$I_{G2}=\pm 10\mu\text{A}$ , $V_{G1S}=0$	$\pm 6.0$			$\pm 6.0$			$\pm 6.0$			volts
VG1S (off)	Gate 1 to Source Cut off Voltage	$V_{DS}=15\text{V}$ , $V_{G2S}=4.0\text{V}$ , $I_D=200\mu\text{A}$	-	-4.0		-	-4.0		-	-4.0		volts
VG2S (off)	Gate 2 to Source Cut off Voltage	$V_{DS}=15\text{V}$ , $V_{G1S}=4.0\text{V}$ , $I_D=200\mu\text{A}$	-	-2.0		-	-3.0		-	-2.0		volts
I <sub>G1SS</sub>	Gate 1-Leakage Current	$V_{G1S}=\pm 4.0\text{V}$ , $V_{G2S}=0$ , $V_{DS}=0$	-	20		-	20		-	20		nAdc
I <sub>G2SS</sub>	Gate 2-Leakage Current	$V_{G2S}=\pm 4.0\text{V}$ , $V_{G1S}=0$ , $V_{DS}=0$	-	20		-	20		-	20		nAdc
I <sub>DSS</sub>	Zero-Gate Voltage Drain Current	$V_{DS}=15\text{V}$ , $V_{G1S}=0$ , $V_{G2S}=4.0\text{V}$	2.0 Note 3	18		5.0 Note 3	30		2.0 Note 3	20		mAdc
Y <sub>fs1</sub>	Fwd. Transadmittance (Gate 1 - Drain)	$V_{DS}=15\text{V}$ , $V_{G2S}=4.0\text{V}$ , $I_D=10\text{mA}$ , $f=1.0\text{kHz}$	10	20		10	20		10	20		mmho
C <sub>iss</sub>	Input Capacitance	$V_{DS}=15\text{V}$	-	7.0		-	6.0		-	7.0		pF
C <sub>oss</sub>	Output Capacitance	$V_{G2S}=4.0\text{V}$	-	3.0		-	3.0		-	3.0		pF
C <sub>rss</sub>	Reverse Transfer Capacitance	$I_D=I_{DSS}$ , $f=1.0\text{MHz}$	-	.03		-	.03		-			pF
NF	Common Source Noise Figure (See Note #1)	$V_{DS}=15\text{V}$ , $V_{G2S}=4.0\text{V}$ , $I_D=6.0\text{mA}$ , $f=105\text{MHz}$	-	2.5	3.5	-	-		-	-		dB
		$f=44\text{MHz}$	-	-	-	-	2.5	3.0	-	-		dB
		$f=200\text{MHz}$	-	-	-	-	3.5	4.0	-	-		dB
G <sub>ps</sub>	Common Source Power Gain (See Note #2)	$V_{DS}=15\text{V}$ , $V_{G2S}=4.0\text{V}$ , $I_D=6.0\text{mA}$	17	22		-	-		-	-		dB
		$f=105\text{MHz}$	-	-	-	-	-		-	-		dB
		$f=44\text{MHz}$	-	-	-	-	30		-	-		dB
		$f=200\text{MHz}$	-	-	-	-	16	19	-	-		dB
G <sub>c</sub>	Common Source Conversion Power Gain	$V_{DD}=15\text{V}$ , Signal Freq.=100MHz, Local Osc. f=110.7MHz	-	-	-	-	-		15	18		dB
		Signal Freq.=200MHz, Local Osc. f=244MHz	-	-	-	-	-		12	15		dB
r <sub>iss</sub>	Input Resistance	$V_{DS}=15\text{V}$ , $V_{G2S}=4.0\text{V}$ , $I_D=6.0\text{mA}$	-	3.2		-	-		-	3.2		kΩ
		$f=105\text{MHz}$	-	-	-	-	-		-	-		kΩ
		$f=44\text{MHz}$	-	-	-	-	15		-	-		kΩ
		$f=200\text{MHz}$	-	-	-	-	0.9		-	0.9		kΩ
r <sub>oss</sub>	output Resistance	$V_{DS}=15\text{V}$ , $V_{G2S}=4.0\text{V}$ , $I_D=6.0\text{mA}$	-	3.5		-	-		-	-		kΩ
		$f=105\text{MHz}$	-	-	-	-	-		-	-		kΩ
		$f=44\text{MHz}$	-	-	-	-	18		-	17		kΩ
		$f=200\text{MHz}$	-	-	-	-	1.5		-	-		kΩ
		$f=10.7\text{MHz}$	-	-	-	-	-		-	30		kΩ
Y <sub>fs</sub>	Magnitude of Fwd Transadmittance	$V_{DS}=15\text{V}$ , $I_D=6.0\text{mA}$ , $V_{G2S}=4.0\text{V}$	-	14		-	-		-	-		mmho
		$f=105\text{MHz}$	-	-	-	-	-		-	-		mmho
		$f=200\text{MHz}$	-	-	-	-	16		-	-		mmho
Y <sub>rs</sub>	Magnitude of Rev Transadmittance	$V_{DS}=15\text{V}$ , $I_D=6.0\text{mA}$ , $V_{G2S}=4.0\text{V}$	-	18		-	-		-	-		μmho
		$f=105\text{MHz}$	-	-	-	-	-		-	-		μmho
		$f=200\text{MHz}$	-	-	-	-	36		-	-		μmho
θ <sub>fs</sub>	Angle of Fwd Transadmittance	$V_{DS}=15\text{V}$ , $I_D=6.0\text{mA}$ , $V_{G2S}=4.0\text{V}$	-	-18		-	-		-	-		degree
		$f=105\text{MHz}$	-	-	-	-	-		-	-		degree
		$f=200\text{MHz}$	-	-	-	-	-35		-	-		degree
θ <sub>rs</sub>	Angle of Rev Transadmittance	$V_{DS}=15\text{V}$ , $I_D=6.0\text{mA}$ , $V_{G2S}=4.0\text{V}$	-	90		-	-		-	-		degree
		$f=105\text{MHz}$	-	-	-	-	-		-	-		degree
		$f=200\text{MHz}$	-	-	-	-	-30		-	-		degree

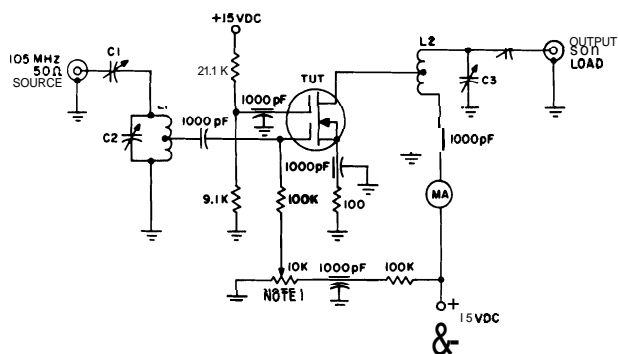
## NOTES:

- Noise Figure: MEM630 See Fig. #1/MEM631 See Fig. #2 and #3
- Power Gain: MEM630 See Fig. #1/MEM631 See Fig. #2 and #3

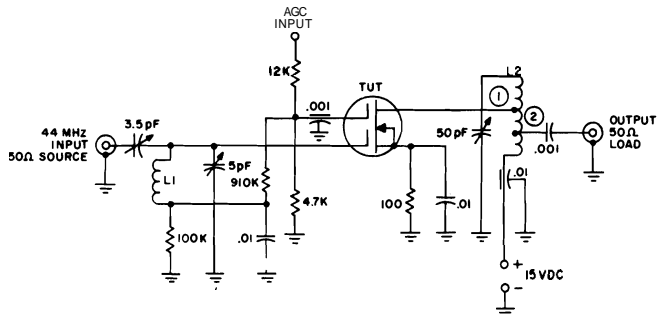
Device	I <sub>DSS</sub> Range (mA)	Color Code	Suggested Source Resistor (ohms)	Suggested Biasing (volts)
MEM630	2-9	Black Dot	150	$V_{G1} = +1.5$
100 MHz R.F. Amplifier	7-18	Blue Dot	180	$V_{G2S} = +4.0$
MEM631	5-13	Black Dot	150*	$V_{G1} = +1.5^*$
200 MHz R.F. Amplifier	11-22	Blue Dot	180*	$V_{G2S} = +4.0^*$
	20-30	Red Dot	200*	
MEM632	2-9	Black Dot	100	$V_{G1} = +0.5$
Mixer	7-14	Blue Dot	100	$V_{G2} = +1.5$
	12-20	Red Dot	100	

\* When the MEM631 is used as an R.F. amplifier, the suggested source resistor is 270 ohms with  $V_{G1} = +1.0$  volts and  $V_{G2S} = +4.0$  volts.

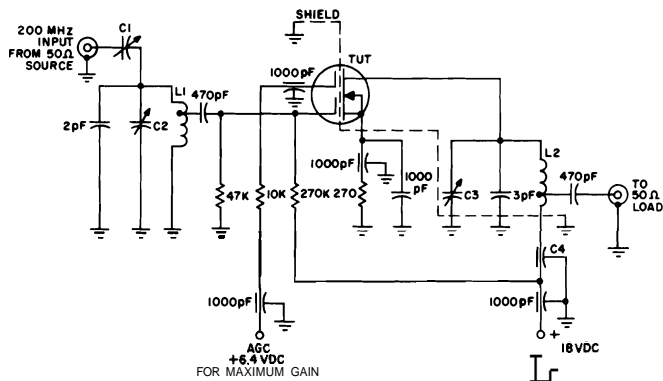
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**Fig. 1 — 105 MHz POWER GAIN/NOISE FIGURE TEST CIRCUIT**


- L1 6T NO.16 BARE COPPER WIRE ON 5/16" DIAM. CORE. 1/2" LONG TAP AT 4-1/21.  
 $C_1 = 17.8\text{pF}$   $R_1 = 15\text{K}$  AT 100MHZ, MOUNTED.
- L2 SAME AS L1, BUT  $R_1 = 30\text{K}$  MOUNTED.
- C1, C4 0.9 TO 7.0pF TRIMMER.
- C2, C3 AIR VARIABLE CAPACITOR 20pF MAX.
- NOTE 1: ADJUST 10K POT. FOR 6mA  $I_D$ .

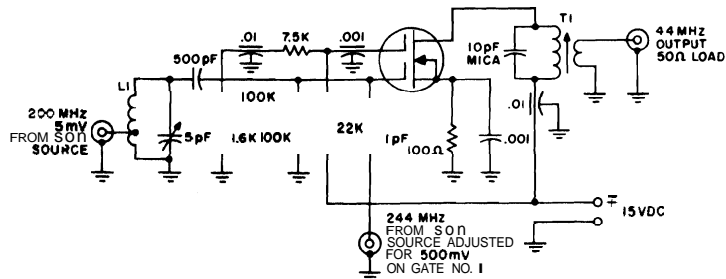
**Fig. 2 — 44 MHz POWER GAIN/NOISE FIGURE TEST CIRCUIT**


- L1 14T NO 32 COTTON COVERED COPPER WIRE CLOSE WOUND ON 1/4" DIAM. FORM
- L2 7T NO 16 BARE COPPER WIRE ON 1/2" FORM. 1/2" WNG  
 DRAIN TAP 2-1/21 FROM COLO END  
 ② LOAD TAP 0.4T FROM COLO END

**Fig. 3 — 200 MHz POWER GAIN/NOISE FIGURE TEST CIRCUIT**


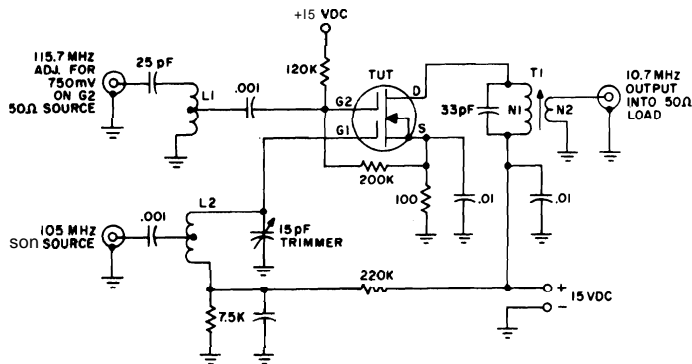
- L1 4T NO.16 BARE COPPER WIRE 3/16" DIAM. FORM. 1/2" LONG TAP AT 3T FROM COLO END.
- L2 4T NO.16 1/4" DIAM. FORM. 1/2" LONG TAP AT 3/4T FROM COLO END.
- C1 0.4 TO 7pF (ARCO 400).
- C2, C3 1.3 TO 5pF VARIABLE.
- C4 1000pF BUTTON TYPE CAPACITOR.
- AGC +6.4VDC FOR MAXIMUM GAIN

Fig. 4 — 200 MHz to 44 MHz MIXER TEST CIRCUIT



- L1 3T NO. 16 BARE COPPER WIRE ON 1/16" CORE. 1/2" LONG TAP AT 3/4T FROM COLD END  
 T1 PRIMARY 10T NO. 32 COTTON COVERED COPPER WIRE CLOSE WOUND ON 1/4" FORM.  
 SECONDARY 1T NO. 32 ENAMELED COPPER WIRE ADJUSTED FOR 16 TO 1 TURNS RATIO.

Fig. 5 — 105 MHz to 10.7 MHz CONVERSION GAIN TEST CIRCUIT (PRODUCT MIXER)



- L1 6T NO. 18 BARF COPPER WIRE ON 5/16" DIAM. CORE. 1/2" LONG TAP AT 2T FROM COLD END.  
 L2 4T NO. 18 BARE COPPER WIRE ON 5/16" DIAM. CORE. 3/8" LONG TAP AT 1T FROM COLD END  
 T1 Q<sub>0</sub> = 67 AT 10.7 MHz, N<sub>1</sub>/N<sub>2</sub> = 17.

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